



PAC addition to remove micropollutants: promising flow schemes

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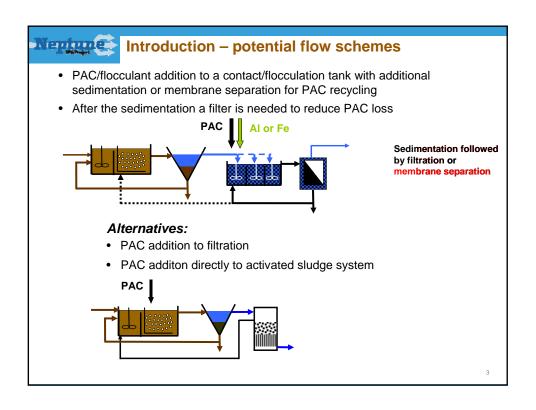
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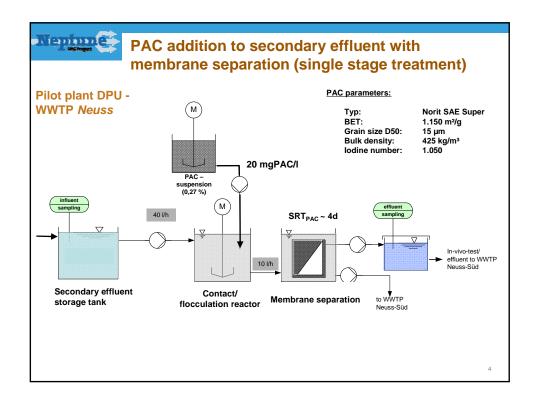


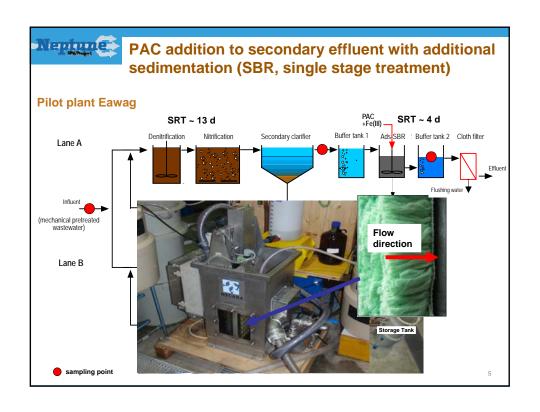
Overview Overview

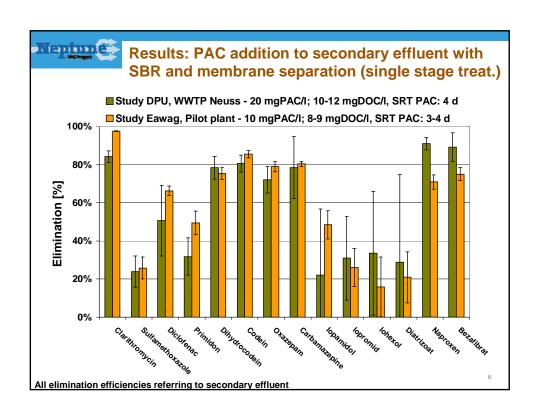
- Introduction: potential flow schemes
- PAC: Results from pilot- and full scale experiments
 - Single stage addition: to effluent or to biology
 - Two stage application: PAC recycling to biology
- Results from GAC application (BioMAC)
- Energy and costs
- Conclusions Outlook

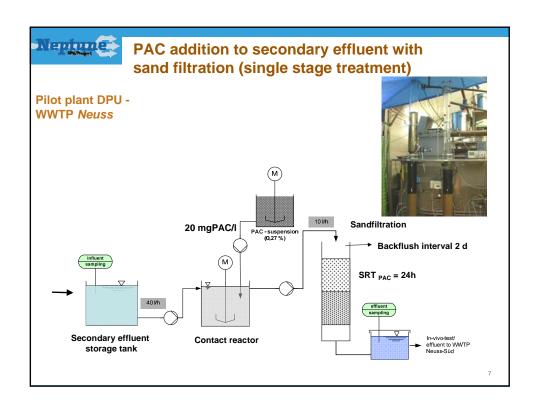
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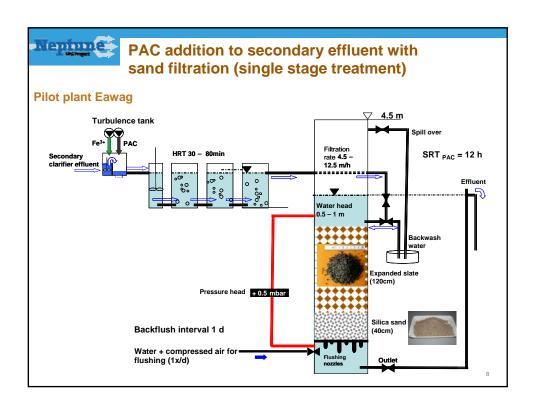


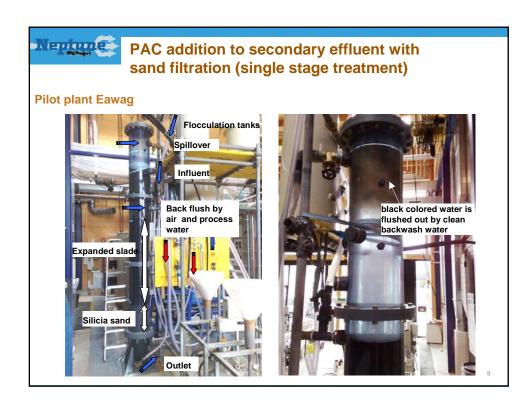












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Full-scale experiments at WWTP Opfikon

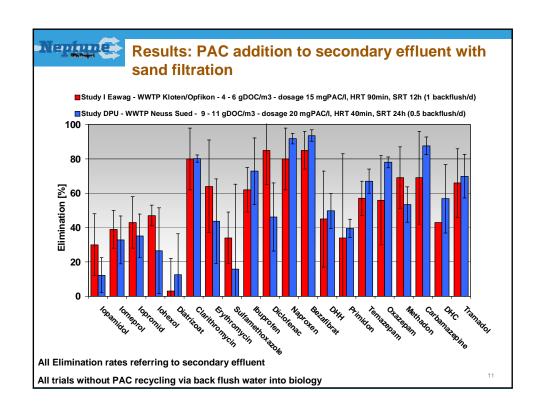
Activated sludge system with two lanes for nitrification and denitrification for 60'000 PE, each lane has two biology tanks with two secondary clarifiers

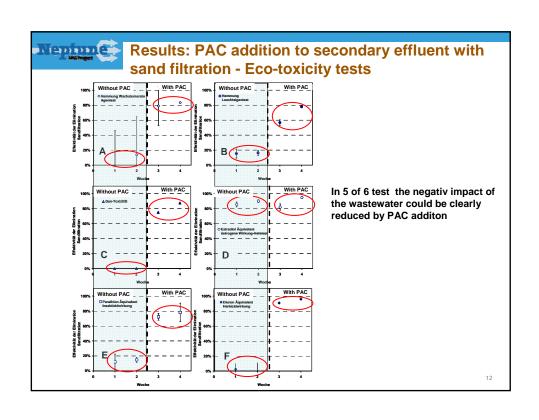
Each lane has one flocculation reactor followed by four two layer filters

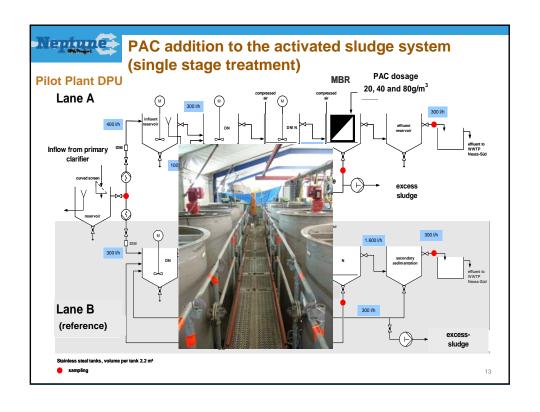
Fe and PAC were only added to the flocculation tank (HRT = 0.9 h) of lane south with one filter in operation (hydraulic load 4.3 m/h, SRT of PAC in the Filter was 12 h, backflush intervall: 1x/d)

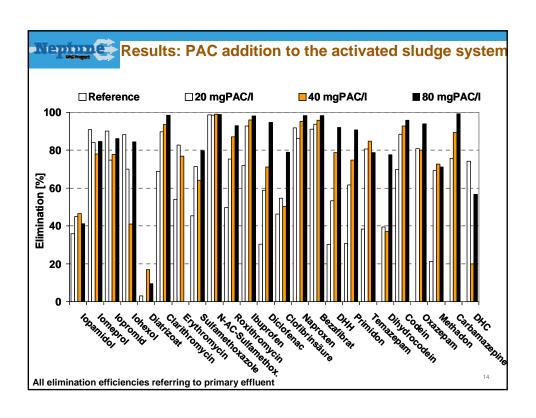


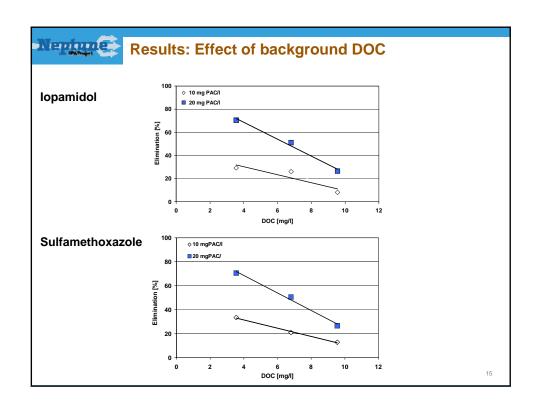
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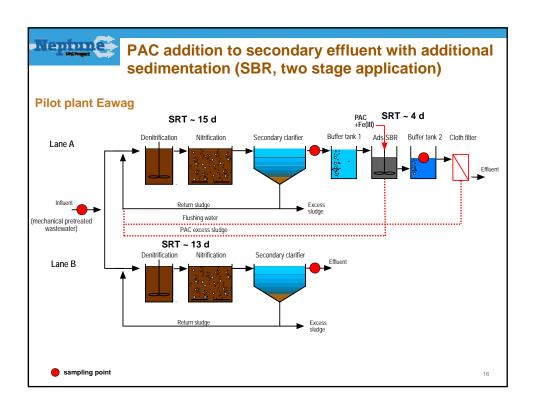


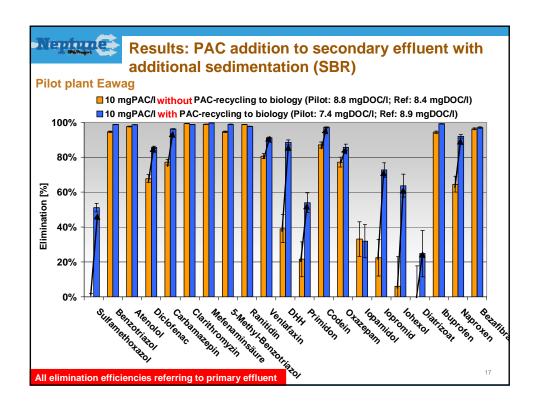


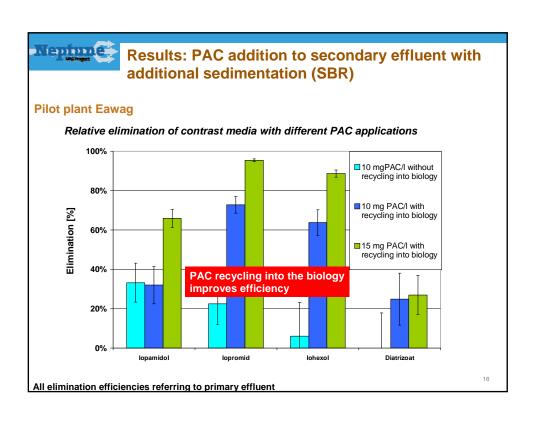


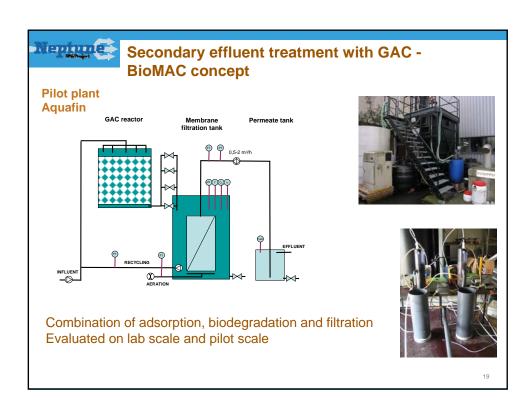


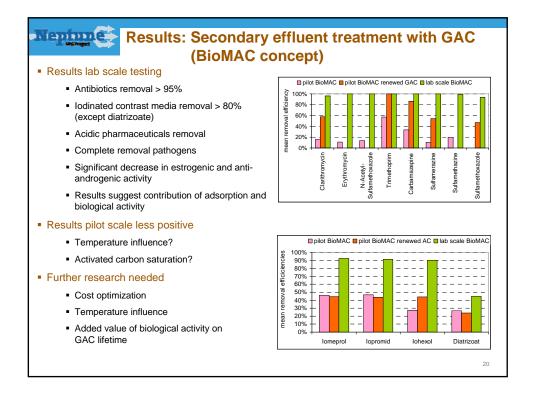














Energy and costs

Treatment	Dosage [mg L ⁻¹]	Electrical energy [kWh m ⁻³ ww]	Primary energy [kWh m ⁻³ ww]	Annual Costs ^c	
				30'000 p.e. [€m ⁻³ ww]	500'000 p.e. [€m ⁻³ ww]
O ₃	3 ^a - 10	0.05 ^b - 0.15	0.15 - 0.45	0.07 ^d - 0.1	0.02 ^d - 0.03
O ₃ incl. sand filter	3 ^a - 10	0.1 - 0.2 ^e	0.3 - 0.6	0.15 ^d - 0.2	0.05 ^d - 0.07
PAC	10 - 20	0.005 ^f	0.35 - 0.7 ^g	0.15 - 0.2	0.06 - 0.08
PAC incl. sand filter	10 - 20	0.05 ^{e,f}	0.5 - 0.8 ^g	0.25 - 0.3	0.09 - 0.11

- ^a Ø Operating conditions @ WWTP Regensdorf (5mg DOC L⁻¹ ≅ 600g O₃ kg⁻¹ DOC)
- b Measured @ WWTP Regensdorf (production of O₃ (incl. O₂), thermal residual-O₃ destructor, control system, cooling aggregate ≈ 15kWh kg⁻¹ O₃)
- ° Detailed, realistic cost study by Hunziker Ltd. (~300L c $^{-1}$ d $^{-1}$ \Rightarrow 100m 3 c $^{-1}$ y $^{-1}$) d extrapolated from O $_3$ 5-10mg L $^{-1}$
- e Sand filter (experience from conventional treatment)
- f Mixing (experience from conventional treatment)
- ⁹ Primary energy consumption of PAC (no regeneration) 3.5 kg carbon needed for 1 kgPAC: $3.5 \text{kgC/kgPAC} \times 2.7 \text{kgCOD/kgC} \times 14 \text{MJ/kgCOD} / 3.6 \text{MJ/kWh} = 35 \text{kWh/kgPAC}$



Conclusions

- Sorption efficiency of PAC reduced with increasing DOC
- ➤ Adequate treatment of secondary effluent requires 10 20 gPAC/m³ depending on DOC background concentration (5 - 10 gDOC/m³) respectively
- ➤ High dosages of PAC (80 gPAC/m³) directly into the activated sludge can not be justified due to the low additional benefit compared to lower dosages (40 gPAC/m³)
- > PAC dosage results in an increase of sludge production of approximately 5-10% (10-20 gPAC/m³)
- Investment and operation costs (incl. filtration) amount to 0.1-0.3 € m⁻³ for PAC addition with flocculation, sedimentation and filtration (~15 - 45 €/(PE·a)
- > PAC recycling into the biology (counterflow) clearly increases elimination efficiency



Outlook

Further tests with pilot plant Eawag

(Winter/Spring 2010)

- Dosage of 20 and 40 mgPAC/l into the biology
- Behaviour of the loaded PAC in the digestion step – desorption of adsorbed micropollutants?
- Batchtests inhibition of the nitrifiers by PAC?

Second full scale application - sandfiltration at WWTP Kloten/Opfikon (Summer 2010) Repetition and optimisation of full scale application at WWTP

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Acknowledgment





This study was part of the EU Neptune project (Contract No 036845, SUSTDEV-2005-3.II.3.2), which was financially supported by grants obtained from the EU Commission within the Energy, Global Change and Ecosystems Program of the Sixth Framework (FP6-2005-Global-4)









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